

VirtualLab Fusion Technology – Solvers and Functions

## **Idealized Grating Functions**

For the Functional Grating Component

#### Abstract

The idealized grating function works without information about the actual shape of the grating structure. In the spatial frequency (k) domain, it defines

- 1. the position (in k domain) of the diffraction orders according to the grating equation, and
- 2. the effective B-matrix for each order according to a desired diffraction efficiency.

The relationship between the position of an arbitrary diffraction order and that of the input is governed by the grating equation. For a specific order, to connect the outgoing electromagnetic field quantities with the incoming ones, a 2×2 B-matrix is needed. An idealized method is used to define such an effective B-matrix from a given diffraction efficiency.



# **Function Algorithm – Grating Equation**

• In the k domain, the grating equation can be expressed as

$$\boldsymbol{\kappa}^{\text{out}} = \boldsymbol{\kappa}^{\text{in}} + j_x \frac{2\pi}{d_x} + j_y \frac{2\pi}{d_y} \,,$$

where

- $\kappa^{\text{out}}$  is the transverse spatial frequency of an arbitrary diffraction order, with order indices  $j_x$  and  $j_y$  along x and y respectively;
- $\kappa^{in}$  is the input transverse spatial frequency;
- $d_x$  and  $d_y$  are the grating periods along x and y respectively.
- From the transverse spatial frequencies, the corresponding diffraction angle can be calculated if needed. In this document we keep working in the k domain and only leave it when required.



illustration of the grating equation in the k domain for a 1D grating along the x direction

### **Function Algorithm – From B-Matrix to Efficiency**

• Let us consider the following input plane wave

$$\boldsymbol{E}_{\perp}^{\mathsf{in}}(\boldsymbol{r}) = \tilde{\boldsymbol{E}}_{\perp}^{\mathsf{in}} \exp(\mathrm{i}\boldsymbol{\kappa}^{\mathsf{in}} \cdot \boldsymbol{\rho}) \exp(\mathrm{i}k_{z}^{\mathsf{in}}z),$$

with given  $\kappa^{\text{in}}$  and  $\tilde{\boldsymbol{E}}_{\perp}^{\text{in}} = (\tilde{E}_x^{\text{in}}, \tilde{E}_y^{\text{in}}).$ 

 For a specific diffraction order, the output plane wave can be expressed as

$$\boldsymbol{E}_{\perp}^{\mathsf{out}}(\boldsymbol{r}) = \tilde{\boldsymbol{E}}_{\perp}^{\mathsf{out}} \exp(\mathrm{i}\boldsymbol{\kappa}^{\mathsf{out}} \cdot \boldsymbol{\rho}) \exp(\mathrm{i}k_{z}^{\mathsf{out}}z),$$

with  $\kappa^{out}$  determined via the grating equation, and the transverse field components connected by a 2×2 B-matrix:

$$\begin{pmatrix} \tilde{E}_x^{\text{out}} \\ \tilde{E}_y^{\text{out}} \end{pmatrix} = \begin{pmatrix} b_{xx} & b_{xy} \\ b_{yx} & b_{yy} \end{pmatrix} \begin{pmatrix} \tilde{E}_x^{\text{in}} \\ \tilde{E}_y^{\text{in}} \end{pmatrix}$$

• For a homogeneous isotropic medium with constant relative permittivity  $\epsilon$  and permeability  $\mu$ , we can calculate

$$k_z = \sqrt{k_0^2 \epsilon \mu - k_x^2 - k_y^2} \,,$$

and

$$\tilde{E}_z = -\frac{k_x\tilde{E}_x + k_y\tilde{E}_y}{k_z}\,.$$

• We restrict ourselves to the case of **lossless** media (real-valued  $\epsilon$  and  $\mu$ ), and in such cases, the time-averaged Poynting vector can be expressed as

$$\boldsymbol{S} = \left\langle \bar{\boldsymbol{S}}^{(\mathsf{r})}(t) \right\rangle = \frac{1}{2\omega\mu_0\mu} ||\tilde{\boldsymbol{E}}||^2 \boldsymbol{k},$$

with its direction coinciding with that of the wavevector k.

• Applying the relation above, the **diffraction efficiency** of a specific order can be calculated (with respect to the input) via

$$\eta = \frac{S_z^{\text{out}}}{S_z^{\text{in}}} = \frac{\mu^{\text{in}} ||\tilde{\boldsymbol{E}}^{\text{out}}||^2 k_z^{\text{out}}}{\mu^{\text{out}} ||\tilde{\boldsymbol{E}}^{\text{in}}||^2 k_z^{\text{in}}},$$

where  $S_z$  and  $k_z$  are the *z* components of the time-averaged Poynting vector and the wavevector respectively.

• Here  $\tilde{E}$  is a three-dimensional vector:

$$ilde{m{E}} = \left( egin{array}{c} ilde{E}_x \ ilde{E}_y \ ilde{E}_z \end{array} 
ight) \,.$$

- From the diffraction efficiency  $\eta,$  we can only conclude the following relation

$$\frac{||\tilde{\boldsymbol{E}}^{\mathsf{out}}||^2}{||\tilde{\boldsymbol{E}}^{\mathsf{in}}||^2} = \frac{\mu^{\mathsf{out}}k_z^{\mathsf{in}}}{\mu^{\mathsf{in}}k_z^{\mathsf{out}}}\eta.$$

- Obviously, the ratio between  $||\tilde{E}^{out}||^2$  and  $||\tilde{E}^{in}||^2$  does NOT fix a unique B-matrix. The solution of the B-matrix in this case is, in general, ambiguous.
- In order to select one possible solution for the B-matrix, additional conditions or constraints must be introduced.
- We assume that the B-matrix is diagonal and identical in the TE-TM coordinate system that is defined by the input and output wavevector directions.
- This is one typical way to define the B-matrix, but not the only way.

- We can generally define the basis vectors of the TE-TM coordinate system, by using the two wavevectors  $k^{in}$  and  $k^{out}$ , as
  - TE (*Y*-direction) :  $\hat{\boldsymbol{Y}} = \hat{\boldsymbol{k}}^{\mathsf{in}} imes \hat{\boldsymbol{k}}^{\mathsf{out}}$ , and
  - TM (X-direction):  $\hat{\boldsymbol{X}}^{\text{in/out}} = \operatorname{sign}(\hat{\boldsymbol{k}}_z^{\text{in/out}}) \left(\hat{\boldsymbol{Y}} \times \hat{\boldsymbol{k}}^{\text{in/out}}\right).$
- In the special case when the relation

$$\hat{m{k}}^{\mathsf{in}}=\pm\hat{m{k}}^{\mathsf{out}}$$

holds, we define the basis vectors as

- TE (*Y*-direction) :  $\hat{Y} = \hat{k}^{in} \times \hat{z}$ , with *z* as the unit direction vector along *z*-direction, and

- TM (X-direction): 
$$\hat{\boldsymbol{X}}^{\text{in/out}} = \operatorname{sign}(\hat{\boldsymbol{k}}_z^{\text{in/out}}) \left(\hat{\boldsymbol{Y}} \times \hat{\boldsymbol{k}}^{\text{in/out}}\right).$$



definition of the basis vectors for the TE-TM coordinate system

• With the basis vectors of the TE-TM coordinate system defined, we can write down the following transformation relations

$$\begin{pmatrix} \tilde{E}_x^{\text{in}} \\ \tilde{E}_y^{\text{in}} \end{pmatrix} = \begin{pmatrix} \hat{X}_x^{\text{in}} & \hat{Y}_x \\ \hat{X}_y^{\text{in}} & \hat{Y}_y \end{pmatrix} \begin{pmatrix} \tilde{E}_X^{\text{in}} \\ \tilde{E}_Y^{\text{in}} \end{pmatrix} ,$$

$$\begin{pmatrix} \tilde{E}_x^{\text{out}} \\ \tilde{E}_y^{\text{out}} \end{pmatrix} = \begin{pmatrix} \hat{X}_x^{\text{out}} & \hat{Y}_x \\ \hat{X}_y^{\text{out}} & \hat{Y}_y \end{pmatrix} \begin{pmatrix} \tilde{E}_X^{\text{out}} \\ \tilde{E}_Y^{\text{out}} \end{pmatrix} .$$

• In the TE-TM system, the B-matrix is expressed in the following simple form:

$$\left(\begin{array}{c} \tilde{E}_{\mathsf{X}}^{\mathsf{out}} \\ \tilde{E}_{\mathsf{Y}}^{\mathsf{out}} \end{array}\right) = \left(\begin{array}{c} B & 0 \\ 0 & B \end{array}\right) \left(\begin{array}{c} \tilde{E}_{\mathsf{X}}^{\mathsf{in}} \\ \tilde{E}_{\mathsf{Y}}^{\mathsf{in}} \end{array}\right) \,.$$



definition of the basis vectors for the TE-TM coordinate system

• In the TE-TM coordinate, it is straight-forward to see that

$$||\tilde{\boldsymbol{E}}^{\mathsf{in}}||^{2} = |\tilde{E}_{\mathsf{X}}^{\mathsf{in}}|^{2} + |\tilde{E}_{\mathsf{Y}}^{\mathsf{in}}|^{2}, \quad ||\tilde{\boldsymbol{E}}^{\mathsf{out}}||^{2} = \left(|\tilde{E}_{\mathsf{X}}^{\mathsf{in}}|^{2} + |\tilde{E}_{\mathsf{Y}}^{\mathsf{in}}|^{2}\right)|B|^{2},$$

and by substituting in the expression of diffraction efficiency, we find that

$$\frac{||\tilde{\boldsymbol{E}}^{\mathsf{out}}||^2}{||\tilde{\boldsymbol{E}}^{\mathsf{in}}||^2} = |B|^2 = \frac{\mu^{\mathsf{out}}k_z^{\mathsf{in}}}{\mu^{\mathsf{in}}k_z^{\mathsf{out}}}\eta,$$

from which the value of |B| can be fixed.

• With the help of the coordinate transformation relations, we can finally write down the relations in the *x*-*y* coordinate system:

$$\left( \begin{array}{c} \tilde{E}_x^{\text{out}} \\ \tilde{E}_y^{\text{out}} \end{array} \right) = B \left( \begin{array}{c} \hat{e}_x^{\text{X,out}} & \hat{e}_x^{\text{Y}} \\ \hat{e}_y^{\text{X,out}} & \hat{e}_y^{\text{Y}} \end{array} \right) \left( \begin{array}{c} \hat{e}_x^{\text{X,in}} & \hat{e}_x^{\text{Y}} \\ \hat{e}_y^{\text{X,in}} & \hat{e}_y^{\text{Y}} \end{array} \right)^{-1} \left( \begin{array}{c} \tilde{E}_x^{\text{in}} \\ \tilde{E}_y^{\text{in}} \end{array} \right) \,.$$

## **Usage in VirtualLab Fusion**

 Idealized grating functions do not require any knowledge about the specific shape of the grating structure, and can be initialized simply with the period value(s).

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## **Usage in VirtualLab Fusion**

- Idealized grating functions do not require any knowledge about the specific shape of the grating structure, and can be initialized simply with the **period** value(s).
- Then, the **indices** of the diffraction orders to be considered and the corresponding **efficiencies** need to be specified in addition.
- The corresponding B-matrix is automatically derived from the diffraction efficiency, by assuming the B-matrix is diagonal and identical in the TE-TM coordiante system.



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